COMPARISON OF DIFFERENT SCALING METHODS FOR MODEL TESTS WITH CLT PROPELLERS

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Energy saving is a primary objective, if not the first and probably still the most important one, especially considering the present worldwide economic crisis, in the design of marine propellers. In parallel to this, the stricter regulations in terms of air pollution, and the lower limits for NO_x and SO_x emissions require ever more efficient designs. CLT propellers represent an opportunity to increase ship propulsion efficiency [1]; however, being unconventional, their design presents larger difficulties, among which the necessity for suitable scaling procedures from model to full scale.

As it is well known, the propulsive performances of a propeller are usually checked by means of Open Water Tests in uniform flow and Self Propulsion Tests with hull; both SPT and OWT are carried out at much lower Reynolds number than full scale, so that model test results are affected by viscous scale effects, and suitable extrapolation procedures are needed.

CLT propellers are affected by larger scale effects than conventional propellers because of the higher tip loading and of the complex phenomena related to the presence of the end plate, with possible separation phenomena at model scale. In order to overcome this issue, SISTEMAR and CEHIPAR have introduced ad hoc corrections to the ITTC 1978 OWT results scaling procedure, taking into account scale effects on lift and viscous forces over the blades and on viscous forces over the end plates [2]. This CLT scaling procedure has been validated and refined by means of the continuous comparison between model and full scale tests, increasing the database for the correlation coefficients and thus the reliability of the procedure.

In present work, possible alternatives to the usually adopted procedure are considered, in order to have a better insight into this phenomenon. In particular, a scaling method, based on the strip method developed by SINM [3] is presented, together with direct calculations in model and full scale made with panel methods developed by UNIGE [4], and with direct computations by a RANS solver made by VTT [5].

The corrections in KT and KQ derived by means of different approaches are compared, considering a reference case, the high speed ferry "Fortuny" of the Spanish company ACCIONA TRASMEDITERRANEA, for which reliable model test and sea trials results with CLT propellers are available thanks to a previous R&D project sponsored by the Spanish authorities in 2003 [6]. This comparison allows to assess the merits and shortcomings of different methods; moreover, the analysis of the numerical calculations adopted allows to obtain a more direct view of the various phenomena typical of the

CLT propellers, gaining further information for the development of suitable scaling procedures.

[1] Gómez, G.P. & González-Adalid, J., "Tip Loaded Propellers (CLT)- Justification of their Advantages over Conventional Propellers Using the New Momentum Theory", SNAME 50th Anniversary, (1942-1992), 1992.

[2] M. Pérez Sobrino; E. Minguito Cardeña; A. García Gómez; J. Masip Hidalgo; R. Quereda Laviña; L. Pangusión Cidales; G. Pérez Gómez; J. González-Adalid. "Scale Effects in Model Tests with CLT Propellers". 27th Motor Ship Marine Propulsión Conference. Bilbao, Spain, 27th-28th January 2005.
[3] "Report 220/07 CLT propellers - Strip Method Estrapolation" SINM internal report 220/07 (and subsequent versions), 15th October 2007.

[4] Bertetta, D., Brizzolara, S., Canepa, E., Gaggero, S. and Viviani, M., "EFD and CFD Characterization of a CLT Propeller", International Journal of Rotating Machinery, Volume 2012, Article ID 348939, 2012 (a).

[5] Sánchez-Caja, A., Sipilä, T., Pylkkänen, J., "Simulation of the Incompressible Viscous Flow around an Endplate Propeller Using a RANSE Solver", 26th Symposium on Naval Hydrodynamics, Rome, Italy, 17-22, 2006.

[6] G. Pérez Gómez; J. González-Adalid; A. García Gómez; J. Masip Hidalgo; R. Quereda Laviña; L. Pangusión Cigales; E. Minguito Cardeña; M. Pérez Sobrino; P. Beltrán Palomo; C. Galindo: "Full scale comparison of a superferry performance fitted with both high skewed and CLT blades". World Maritime Technology Conference, March 2006